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(ii) Process and catalyst for producing reactor blend polyolefins.

57 Polyolefin reactor blends obtained by polymerization of ethylene and higher alpha-olefins in the presence of a catalyst system comprising two or more metallocenes and alumoxane.

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PROCESS AND CATALYST FOR PRODUCING REACTOR BLEND POLYOLEFINS

The present invention concerns catalyst and process for the polymerization of ethylene and alpha-olefins. More particularly, the invention relates to catalysts and process for producing (co)polyolefin reactor blends of ethylene and ethylene-alpha-olefin copolymers. The invention further relates to a process for producing tailored (co)polyolefins reactor blends through the proper selections of the catalysts of this invention.

Reactor blends for purposes of this invention are mixtures of two or more polymers of different physical properties (density, melting point, comonomer content, etc.) produced simultaneously in a single polymerization reactor. Catalyst employed in the production of such polymer blends under steady state conditions in one reactor will comprise two or more distinct catalyst components, one predominately catalyzing the formation of one polymer, the other predominately catalyzing the formation of the other polymer.

DESCRIPTION OF THE PRIOR ART

It is known that certain metallocenes such as bis(cyclopentadienyl) titanium and zirconium dialkyls in combination with aluminum alkyl co-catalyst, form homogeneous catalyst systems useful for the polymerization of ethylene. German Patent Application 2,608,863 discloses the use of a catalyst system for the polymerization of ethylene consisting of bis(cyclopentadienyl) titanium dialkyl, aluminum trialkyl and water. German Patent Application 2,608,933 discloses an ethylene polymerization catalyst system consisting of (1) zirconium metallocenes of the general formula (cyclopentadienyl) Try_{4-n}, wherein n stands for a number in the range of 1 to 4, Y for R, CH₂AlR₂, CH₂CH₂AlR₂ and CH₂CH(AlR₂)₂ wherein R stands for alkyl or metallo alkyl, (2) an alumiunum trialkyl cocatalyst and (3) water.
European Patent Appln. No. 0035242 discloses a process for

preparing ethylene and atactic propylene polymers in the

presence of a halogen-free Ziegler catalyst system of (1)
cyclopentadienyl compound of the formula
(cyclopentadienyl)_nMeY_{4-n} in which n is an integer from 1
to 4, Me is a transition metal, especially zirconium, and Y is
either hydrogen, a C₁-C₅ alkyl or metallo alkyl group or a
compound having the following general formula: CH₂AlR₂,
CH₂CH₂AlR₂ and CH₂CH(AlR₂)₂ in which R represents a
C₁-C₅ alkyl or metallo alkyl group, and (2) an alumoxane.

The above disclosures demonstrate the usefulness of certain metallocenes in combination with certain aluminum compounds for the polymerization of ethylene and particularly polymerization at a high activity rates. The references neither disclose polyethylene/copolyethylene-alpha-olefin reactor blends nor methods of producing such reactor blends.

In "Molecular Weight Distribution And Stereoregularity Of Polypropylenes Obtained With Ti(OC₄H₉)₄/Al(C₂H₅)₃ Catalyst System"; Polymer, Pg. 469-471, 1981, Vol. 22, April, Doi, et al disclose propylene polymerization with a catalyst which at about 41°C obtains a soluble catalyst and insoluble catalyst fraction, one with "homogeneous catalytic centres" and the other with "heterogeneous catalytic centres". The polymerization at that temperature obtains polypropylene having a bimodal molecular weight distribution.

It is also known to produce polymer blends by polymerizing two or more polymerizable materials in two or more reactors arranged in series. In accordance with such methods, a polymerizate is produced in a first reactor which first polymerizate is passed to a second reactor wherein a second polymerizate is produced thereby obtaining a blend of the first and second polymerizates.

It is highly desirable to be able to readily and simply produce blends in a single reactor during which polyethylene and copolyethylene-alpha-olefins are produced simultaneously. Not only is a significant reduction in energy costs obtained, but one obtains a uniform blending of the polymers and one can simply "tailor" the polymers with respect to molecular weights,

weight fraction and the like to obtain blends evidencing outstanding properties.

In view of the foregoing problems, it would be highly desirable to provide a polymerization catalyst system of sufficient activity to produce high quality blends of ethylene-alpha olefin polymers. It is furthermore highly desirable to be able to produce the blends of ethylene-alpha olefin polymers directly in a single reactor.

The present invention provides a process for producing (co)polyolefin reactor blends comprising polyethylene and copolyethylene-alpha-olefins. The reactor blends are obtained directly during a single polymerization process, i.e., the blends of this invention are obtained in a single reactor by simultaneously polymerizing ethylene and copolymerizing ethylene with an alpha-olefin thereby eliminating expensive blending operations. The invention furthermore provides a catalyst system for the polymerization of ethylene and ethylene copolymers simultaneously to provide polyethylene blends. The process of producing reactor blends in accordance with this invention can be employed in conjunction with other prior art blending techniques, for example the reactor blends produced in a first reactor can be subjected to further blending in a second stage by use of a series of reactors.

Accordingly, there is provided a catalyst system for the polymerization of reactor blends of polyethylene with ethylene-alpha-olefin copolymers; said catalyst system comprising (a) at least two different metallocenes and (b) an alumoxane. The metallocenes employed in this invention are organometallic coordination compounds which are cyclopentadienyl derivatives of a transition metal of Groups 4b, 5b and 6b and include mono, di and tricyclopentadienyls and their derivatives of the transition metal. The metallocenes can be represented by the general formula

 $(C_5R'_m)_DR''_s(C_5R'_m)MeQ_{3-D}$ or $R''_s(C_5R'_m)MeQ'$, wherein (C₅R'_m) is a cyclopentadienyl or substituted cyclopentadienyl, each R', which can be the same or different, is hydrogen or a hydrocarbyl radical such as alkyl, alkenyl, aryl, alkylaryl, or arylalkyl radical having from 1 to 20 carbon atoms or two R' substituents together form a fused CA-Cc ring, R" is a C1-CA alkylene radical, a dialkyl germanium or silicone, or an alkyl phosphine or amine radical bridging two ($C_5R'_m$) rings, Q is a hydrocarbon radical such as aryl, alkyl, alkenyl, alkylaryl, or arylalkyl radical having from 1 to 20 carbon atoms or halogen and each Q can be the same or different, Q' is an alkylidene radical having from 1 to about 20 carbon atoms. He is a transition metal of Group 4b, 5b, 6b of the Periodic Table (Chemical Rubber Company's Handbook of Chemistry & Physics, 48th Edition), s is 0 or 1, p is 0, 1 or 2: when p = 0, s = 0; m is 4 when s is 1 and m is 5 when s is 0. The ratios of one metallocene to the second metallocene will be a function of both the chemical composition of the metallocenes as well as the blend being tailored; accordingly, the ratio of the two metallocenes can vary greatly and, hence, is limited only for the purpose of producing the blends.

The present invention also provides a process for producing polyolefin reactor blends. The process comprises polymerizing ethylene and higher alpha-olefins in the presence of the catalyst system described above.

DETAILED DESCRIPTION OF THE INVENTION

The present invention is directed towards a catalytic process for the polymerization of ethylene and one or more alpha-olefins to polyethylene-copolyethylene-alpha-olefin reactor blends. The polymers are intended for fabrication into articles by extrusion, injection molding, thermoforming, rotational molding, and the like. In particular, the polymer blends of this invention are blends of polyethylenes such as high density polyethylene (HDPE) and linear low density polyethylene (LLDPE) and with copolyethylene higher alpha-olefins having from 3 to about 10 carbon atoms and

preferably 4 to 8 carbon atoms. Illustrative of the higher alpha-olefins are propylene, butene-1, hexene-1 and octene-1. Preferably, the alpha-olefin is propylene or butene-1.

In the process of the present invention, ethylene, together with the alpha-olefins, is polymerized in the presence of a homogeneous catalyst system comprising at least two different metallocenes and an alumoxane.

The alumoxanes are well known in the art and are polymeric aluminum compounds which can be represented by the general formulae $(R-Al-0)_n$ which is a cyclic compound and $R(R-Al-0-)_nAlR_2$, which is a linear compound. In the general formula R is a C_1-C_5 alkyl group such as, for example, methyl, ethyl, propyl, butyl and pentyl and n is an integer from 1 to about 20 and preferably from about 1 to about 4. Most preferably, R is methyl and n is 4. Generally, in the preparation of alumoxanes from, for example, aluminum trimethyl and water, a mixture of the linear and cyclic compounds are obtained.

The alumoxane can be prepared in various ways. Preferably, they are prepared by contacting water with solution of aluminum trialkyl, such as, for example, aluminum trimethyl, in a suitable organic solvent such as benzene or an aliphatic hydrocarbon. For example, the aluminum alkyl is treated with water in form of a moist solvent or the aluminum alkyl such as aluminum trimethyl can be desirably contacted with a hydrated salt such as hydrated copper sulfate.

Preferably, the alumoxane is prepared in the presence of a hydrated copper sulfate. The method comprises treating a dilute solution of aluminum trimethyl in, for example, toluene, with copper sulfate represented by the general formula CuSO₄.5H₂O. The ratio of copper sulfate to aluminum trimethyl is desirably about 1 mole of copper sulfate for 5 moles of aluminum trimethyl. The reaction is evidenced by the evolution of methane.

The dual metallocene system usefully employed in accordance with this invention are the mono, di and tricyclopentadienyl or substituted cyclopentadienyl metallocenes and preferably the

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titanium (IV) and zirconium (IV) metallocenes. The
1
     metallocenes are represented by the general formula
2
      (C_5R'_m)_pR''_s(C_5R'_m)MeQ_{3-p} and
3
      R_{S}(C_{S}R_{m})_{2}MeQ' wherein (C_{S}R_{m}) is cyclopentadienyl
4
      or substituted cyclopentadienyl, each R' is the same or
5
      different and is hydrogen or a hydrocarbyl radical such as
6
      alkyl, alkenyl, aryl, alkylaryl, or arylalkyl radicals
7
      containing from 1 to 20 carbon atoms or two-carbon atoms are
8
      joined together to form a C_4-C_6 ring, R^{**} is a C_1-C_4
      alkylene radical, a dialkyl germanium or silicone, or an alkyl
10
      phosphine or amine radical bridging two (CgR'm) rings, Q is
11
      a hydrocarbyl radical such as aryl, alkyl, alkenyl, alkylaryl,
12
      or arylalkyl radical having from 1-20 carbon atoms or halogen
13
      and can be the same or different, Q' is an alkylidene radical
14
      having from 1 to about 20 carbon atoms, s is 0 or 1, p is 0, 1
15
      or 2; when p is 0, s is 0, m is 4 when s is 1 and m is 5 when s
16
      is O and Me is a Group 4b, 5b or 6b transition metal and most
17
       preferably zirconium or titanium.
18
           Exemplary hydrocarbyl radicals are methyl, ethyl, propyl,
19
       butyl, amyl, isoamyl, hexyl, isobutyl, heptyl, octyl, nonyl,
20
       decyl, cetyl, 2-ethylhexyl, phenyl, and the like.
21
           Exemplary alkylene radicals are methylene, ethylene,
22
       propylene, and the like.
23
           Preferred examples of substituent Q are methyl,
24
       phenyl or chloride.
25
           Exemplary halogen atoms include chlorine, bromine
26
       and iodine and of these halogen atoms, chlorine is
27
       preferred.
28
           Exemplary of the alkylidene radicals are methylidene,
29
       ethylidene and propylidene.
 30
           Preferably the catalyst comprises at least two
 31
        zirconocenes or at least one titanocene and at least one /
 32
 33
        zirconocene.
           Illustrative but non-limiting examples of the titano-
 34
        cenes which can be usefully employed in accordance with
 35
        this invention are bis(cyclopentadienyl) titanium
 36
```

- 1 diphenyl, the carbene represented by the formula
- 2 Cp₂Ti=CH₂ · Al(CH₃)₂Cl, and derivatives of this
- 3 reagent such as Cp_Ti=CH2 'Al(CH3)3,
- 4 (Cp₂TiCH₂)₂, Cp₂TiCH₂CH(CH₃)CH₂,
- 5 Cp₂Ti=CHCH₂CH₂, Cp₂Ti=CH₂ 'AlR'''₂Cl, wherein Cp
- 6 is a cyclopentadienyl or substituted cylopentadienyl
- 7 radical,

```
and R'" is an alkyl, aryl or alkylaryl radical having from
1
      1-18 carbon atoms; substituted bis(Cp)Ti(IY) compounds such as
2
      bis(indenyl)Ti diphenyl or dichloride,
3
      bis(methylcyclopentadienyl) Ti diphenyl or dihalides and other
4
       dihalide complexes: dialkyl, trialkyl, tetra-alkyl and
5
       penta-alkyl cyclopentadienyl titanium compounds such as
6
       bis(1.2-dimethylcyclopentadienyl)Ti diphenyl or dichloride,
7
       bis(fluorenyl)Ti dichloride, bis(1,2-diethylcyclopentadienyl)Ti
8
       diphenyl or dichloride and other dihalide complexes; silicone,
9
       phosphine, amine or carbon bridged cyclopentadiene complexes,
10
       such as dimethyl silyldicyclopentadienyl titanium diphenyl or
11
       dichloride, methyl phosphine dicyclopentadienyl titanium
12
       diphenyl or dichloride, methylenedicyclopentadienyl titanium
13
       diphenyl or dichloride and other dihalide complexes.
14
           Illustrative but non-limiting examples of the zirconocenes
15
       which can be usefully employed in accordance with this
16
       invention are bis(cyclopentadienyl)zirconium diphenyl.
17
       bis(cyclopentadienyl)zirconium dimethyl; the alkyl substituted
18
       cyclopentadienes, such as bis(ethyl cyclopentadienyl)zirconium
19
       dimethyl, bis(β-phenylpropylcyclopentadienyl)zirconium
20
       dimethyl, bis(methylcyclopentadienyl)zirconium dimethyl and
21
       dihalide complexes of the above; di-alkyl, tri-alkyl,
 22
       tetra-alkyl, and penta-alkyl cyclopentadienes, such as
 23
        bis(pentamethylcyclopentadienyl)zirconium dimethyl, bis
 24
        (1,2-dimethylcyclopentadienyl)zirconium dimethyl,
 25
        bis(1,3-diethylcyclopentadienyl)zirconium dimethyl and dihalide
 26
        complexes of the above; silicone, phosphorus, and carbon
 27
        bridged cyclopentadiene complexes such as
 28
        dimethylsilyldicyclopentadienyl zirconium dimethyl or dihalide.
 29
        methylphosphine dicyclopentadienyl zirconium dimethyl or
 30
        dihalide, and methylene dicyclopentadienyl zirconium dimethyl
 31
        or dihalide, carbenes represented by the formulae
 32
        Cp_2Zr=CH_2P(C_6H_5)_2CH_3, and derivatives of these
 33
        compounds such as Cp_ZrCH_CH(CH_3)CH_2.
 34
              The ratio of aluminum in the alumoxane to total metal in
  35
                                                       0.5:1 to
        the metallocenes can be in the range of
  36
        10<sup>5</sup>:1, and preferably
  37
                                     5:1 to
                                                 1000:1. The molar
```

 ratio of the metallocenes can vary over a wide range and in accordance with this invention the molar ratios are controlled by the product polymer blend desired.

The reactivity ratios of the metallocenes in general are obtained by methods well known such as, for example, as described in "Linear Method for Determining Monomer Reactivity Ratios in Copolymerization", M. Fineman and S. D. Ross, J. Polymer Science 5, 259 (1950) or "Copolymerization", F. R. Mayo and C. Walling, Chem. Rev. 46, 191 (1950) incorporated herein in its entirety by reference. For example, to determine reactivity ratios the most widely used copolymerization model is based on the following equations:

13
$$M_1^* + M_1 - \frac{k_{11}}{k_{12}} M_1^*$$
 (1)
14 $M_1^* + M_2 - \frac{k_{12}}{k_{21}} M_2^*$ (2)
15 $M_2^* + M_1 - \frac{k_{21}}{k_{22}} M_1^*$ (3)
16 $M_2^* + M_2 - \frac{k_{22}}{k_{22}} M_2^*$ (4)

where M_i refers to a monomer molecule which is arbitrarily designated i (where i = 1, 2) and M_2 * refers to a growing polymer chain to which monomer i has most recently attached.

The kij values are the rate constants for the indicated reactions. Thus, k_{11} represents the rate at which an ethylene unit inserts into a growing polymer chain in which the previously inserted monomer unit was also ethylene. The reactivity rates follow as: $r_1=k_{11}/k_{12}$ and $r_2=k_{22}/k_{21}$ wherein k_{11} , k_{12} , k_{22} and k_{21} are the rate constants for ethylene (1) or propylene (2) addition to a catalyst site where the last polymerized monomer is an ethylene (k_{1x}) or propylene (k_{2x}) .

In Table I the ethylene-propylene reactivity rates $\mathbf{r_1}$ and $\mathbf{r_2}$ are listed for several metallocenes. It can be seen that with increased steric interaction at the monomer coordination site $\mathbf{r_1}$ increases, i.e. the tendency for ethylene polymerization increases over propylene polymerization.

1	It can be seen from Table		
2	comprising HDPE/ethylene-propy	lene copolym	er one would select
3	bis(pentamethylcyclopentadieny	1)ZrCl ₂ and	
4	bis(cyclopentadienyl)Ti diphen	yl or	
5	dimethylsilyldicyclopentadieny	l zirconium	dichloride in ratios
6	of 5:1 to 1:1 when	eas if one o	desires a blend
7	comprising LLDPE/ethylene-prop	ylene one w	ould select
8	bis(cyclopentadienyl)Zr dimetl		
9	bis(methylcyclopentadienyl)Zr	12 and bist	cyclopentadienyl)Ti
10	diphenyl or dimethylsilyldicy	lopentadien	yl ZrCl ₂ in ratios
11	of 10:1 to1:1.		
12	Desirably, the metallocen	e molar rati	o will be 100:1
13 .	to 1:100, and preferabl		
14	specific metallocenes selecte		
15	depended upon the molecular c		
16	component polymers and the ov		
17	blend. In general, the compo		
18	blend catalyst mixture will e		
19	different in order to produce	final polym	mer compositions which
20	comprise blends of two or mor	e polymers.	•
20 21	•	e polymers. TABLE I	•
	•	TABLE I	
	•		r ₂
21		rable I	r 2
21		r ₁	r ₂
21	Catalyst	FABLE I F1 24 19.5 <u>+</u> 1.5	r ₂ 0.0085 0.015 <u>+</u> .002
21 22 23	Catalyst Cp ₂ Ti=CH ₂ Al(Me) ₂ Cl	T1 24 19.5+1.5 24+2	r ₂ 0.0085 0.015+.002 0.029+.007
21 22 23 24	Catalyst Cp ₂ Ti=CH ₂ Al(He) ₂ Cl Cp ₂ TiPh ₂	71 24 19.5+1.5 24+2 48+2	r ₂ 0.0085 0.015 <u>+</u> .002
21 22 23 24 25	Catalyst Cp ₂ Ti=CH ₂ *Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂	P1 24 19.5+1.5 24+2 48+2 60	r ₂ 0.0085 0.015±.002 0.029±.007 0.015±.003
21 22 23 24 25 26	Catalyst Cp ₂ Ti=CH ₂ *Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂	TABLE I 24 19.5+1.5 24+2 48+2 60 250+30	°2 0.0085 0.015±.002 0.029±.007 0.015±.003
21 22 23 24 25 26 27	Catalyst Cp ₂ Ti=CH ₂ Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₃ 0	FABLE I 24 19.5+1.5 24+2 48+2 60 250+30 50	r ₂ 0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007
21 22 23 24 25 26 27 28	Catalyst Cp ₂ Ti=CH ₂ 'Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₂ 0 The solvents used in the	71 24 19.5+1.5 24+2 48+2 60 250+30 50 preparation	72 0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007 n of the catalyst system
21 22 23 24 25 26 27 28 29	Catalyst Cp ₂ Ti=CH ₂ 'Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₂ The solvents used in the are inert hydrocarbons, in	71 24 19.5+1.5 24+2 48+2 60 250+30 50 e preparation	r ₂ 0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007 n of the catalyst system hydrocarbon that is
21 22 23 24 25 26 27 28 29 30	Catalyst Cp ₂ Ti=CH ₂ 'Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₂ The solvents used in the are inert hydrocarbons, in inert with respect to the c	71 24 19.5+1.5 24+2 48+2 60 250+30 50 e preparation particular a	0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007 n of the catalyst system hydrocarbon that is em. Such solvents are
21 22 23 24 25 26 27 28 29 30 31	Catalyst Cp ₂ Ti=CH ₂ 'Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₂ 0 The solvents used in the are inert hydrocarbons, in inert with respect to the cowell known and include, for	TABLE I 24 19.5+1.5 24+2 48+2 60 250+30 50 e preparation particular a atalyst syst example, is	0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007 n of the catalyst system hydrocarbon that is em. Such solvents are obutane, butane,
21 22 23 24 25 26 27 28 29 30 31 32	Catalyst Cp ₂ Ti=CH ₂ 'Al(Me) ₂ Cl Cp ₂ TiPh ₂ Me ₂ SiCp ₂ ZrCl ₂ Cp ₂ Zr Cl ₂ (MeCp) ₂ ZrCl ₂ (Me ₅ Cp) ₂ ZrCl ₂ [Cp ₂ ZrCl] ₂ The solvents used in the are inert hydrocarbons, in inert with respect to the c	TABLE I 24 19.5+1.5 24+2 48+2 60 250+30 50 e preparation particular a atalyst syst example, is ctane, cyclo	0.0085 0.015±.002 0.029±.007 0.015±.003 .002±0.001 0.007 n of the catalyst system hydrocarbon that is em. Such solvents are obutane, butane, shexane,

The catalyst systems described herein are suitable for 1 producing polymer product blends in solution, slurry or a gas 2 phase polymerizations and over a wide range of temperatures and 3 pressures. For example, such temperatures may be in the range 4 280°C and especially in the range of -60 to 5 of 160 °C. The pressures employed in the 50 to 6 process of the present invention are those well known for 7 500 atmospheres and 1 to example, in the range of 8 greater. 9 In a solution phase polymerization the alumoxane and 10 metallocene can be employed as a homogeneous catalyst system. 11 The alumoxane is preferably dissolved in a suitable solvent, 12 typically in inert hydrocarbon solvent such as toluene, xylene, 13 0.1 to 3.0. and the like in molar concentations of 14 however greater or lesser amounts can be employed. 15 The soluble metallocenes can be converted to supported 16 heterogeneous catalyst by depositing said metallocenes on 17 typical catalyst supports such as, for example, silica, 18 alumina, and polyethylene. The solid catalysts in combination 19 with an alumoxane can be usefully employed in slurry and gas 20 phase olefin polymerizations. 21 After polymerization and deactivation of the catalyst, the 22 product polymer blend can be recovered by processes well known 23 in the art for removal of deactivated catalysts and solution. 24 The solvents may be flashed off from the polymer solution and 25 the polymer obtained extruded into water and cut into pellets 26 or other suitable comminuted shapes. 27 Pigments, antioxidants and other additives, as is known in 28 29 the art, may be added to the polymer. The polymer product obtained in accordance with this 30 invention will have a weight average molecular weight in the 31 2,000,000 and preferably 10,000 to 500 to : 32 500,000. The component polymers in the reactor blend can **33** have the same or different average molecular weights and 34 comonomer composition; however, it is preferable for most end 35 uses that the average molecular weights and comonomer 36 composition be different. 37

Illustrative, but nonlimiting examples of reactor blends
which can be produced in accordance with this invention are
HDPE/EPR copolymer, LLDPE/EPR copolymer, HDPE/LLDPE and
HDPE/LLDPE/EPR copolymer blends. These polymers demonstrate
superior properties such as for example impact resistance and
tear strength and process more easily than the individual
component polymers.

The polymers produced by the process of this present invention are capable of being fabricated into a wide variety of articles, as is known for blend of ethylene and copolymers of ethylene and higher alpha-olefins. The present invention is illustrated by the following examples.

EXAMPLES

following manner:

In the examples following the molecular weights were determined on a Water's Associates Model No. 150C GPC. The measurements were made by dissolving polymer samples in hot trichlorobenzene (TCB) and filtered. The GPC (Gel Permeation Chromotography) runs were performed at 145°C in TCB at 1.5° ml/min using two Shodex A80M/S columns of 9.4 mm internal diameter from Perkins Elmer Inc. 300 milliliter of 3.1 percent solutions in TCB were injected and the chromotographic runs monitored at sensitivity equal -64 and scale factor equal 65. The samples were run in duplicate. The integration parameters were obtained with a Water's Associates data module. An antioxidant, N-phenyl-2-naphthylamine, was added to all samples. In the examples following the alumoxane was prepared in the

600cc of a 14.5% solution of trimethylaluminum (TMA) in heptane was added in 30cc increments at 5 minute intervals, with rapid stirring, to 200cc toluene in a Zipperclave reactor under nitrogen and maintained at 100°C. Each increment was immediately followed by the addition of 0.3cc water. The reactor was vented of methane after each addition. Upon completion of the addition, the reactor was stirred for 6 hours while maintaining the temperature at 100°C. The mixture,

containing soluble alumoxane is allowed to cool to room 1 temperature and settle. The clear solution containing the 2 soluble alumoxane is separated by decantation from the solids. 3

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Example 1(a) - Reactor blend

A 1-liter stainless steel pressure vessel, equipped with an 6 7 incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply 8 of dry ethylene, propylene and nitrogen, was dried and 9 deoxygenated with a nitrogen flow. 400cc of dry, degassed 10 toluene was introduced directly into the pressure vessel. 25cc 11 of 0.64 molar (in total aluminum) alumoxane was injected into 12 the vessel by a gas tight syringe through the septum inlet and 13 the mixture was stirred at 1,200 rpms and 50°C for 5 minutes 14 at zero (0) psig of nitrogen. 1.12 mg bis(cyclopentadienyl) 15 titanium phenyl dissolved in 2.0 ml of dry, distilled toluene 16 was injected through the septum inlet into the vessel. 17 Similarly, 0.107 mg. bis(pentamethylcylcopentadienyl) zirconium 18 dimethyl in 2.0 ml dry, distilled toluene was injected. The 19 solution was saturated with 200cc propylene at a pressure of 20 165 psig. Thereafter ethylene at 25 psig was passed into the 21 vessel for 60 minutes while maintaining the temperature at 22 50°C at which time the reaction was stopped by rapidly 23 venting and cooling. The copolymer was evaporated to dryness, · 24 weighed and analyzed by GPC and IR. 62 gms of a blend of 25 polyethylene and EPR copolymer which analyzed for 6 mole % 26 propylene and having a Mn of 16,500 and a Mw of 41,800 was 27 28 recovered.

Example 1(b) - Use of One Metallocene -29

bis(pentamethylcyclopentadienyl)Zirconiumdimethyl

30 A 1-liter stainless steel pressure vessel, equipped with an 31 incline blade stirrer, an external water jacket for temperature 32 control, a septum inlet and vent line, and a regulated supply 33 of dry ethylene, propylene and nitrogen, was dried and 34 deoxygenated with a nitrogen flow. 400cc of dry, degassed 35

toluene was introduced directly into the pressure vessel. 25cc 1 of 0.64 molar (in total aluminum) alumoxane was injected into 2 the vessel by a gas tight syringe through the septum inlet and 3 the mixture was stirred at 1,200 rpms and 50°C for 5 minutes 4 at zero (0) psig of nitrogen. 0.122 mg 5 bis(pentamethylcyclopentadienyl)zirconium dimethyl dissolved in 6 2.0 ml of dry, distilled toluene was injected through the 7 septum inlet into the vessel. Liquid propylene (200cc) was 8 added from a calibrated addition vessel resulting in a 9 propylene pressure of 153 psig. Thereafter ethylene at 25 psig 10 was passed into the vessel for 90 minutes while maintaining the 11 temperature at 50°C at which time the reaction was stopped by 12 rapidly venting and cooling. 76 gms of polyethylene which 13 analyzed for 3.4% propylene and having a Mn of 15,300 and a Mw 14 of 36,400 was recovered. The analysis was performed as in 15 Example 1(a). 16

Example 1(c) - Use of One Metallocene bis(cyclopentadienyl)Tidiphenyl

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A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry, degassed toluene was introduced directly into the pressure vessel. 25cc of 0.64 molar (in total aluminum) alumoxane was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 50°C for 5 minutes at zero (0) psig of nitrogen. 1.04 mg bis(cyclopentadienyl) titanium phenyl dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Liquid propylene (200cc) was added from a calibrated addition vessel resulting in a propylene pressure of 165 psig. Thereafter ethylene at 25 psig was passed into the vessel for 90 minutes while maintaining the temperature at 50°C at which time the reaction was stopped by rapidly venting and cooling. 14.4 gms of polyolefin which analyzed for 65% ethylene and 35% propylene and having a Mn of 45,400 and a Hw of 137,000 was recovered.

The analysis was performed as in Example 1(a).

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Example 2 - Use of Two Different Metallocenes

A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry. degassed toluene was introduced directly into the pressure vessel. 10.0cc of 0.83 molar (in total aluminum) alumoxane was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 80°C for 5 minutes at zero (0) psig of nitrogen. 2.127 mg bis(pentamethylcyclopentadienyl) zirconium dichloride dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Similarly, 0.2628 mg bis(methylcyclopentadienyl) zirconium dichloride in 0.25 ml dry, distilled toluene was injected. The solution was saturated with propylene at a pressure of 111 psig for 15 seconds. Thereafter ethylene at 15 psig was passed into the vessel for 20 minutes while maintaining the temperature at 80° C and the pressure at 126° psig at which time the reaction was stopped by rapidly venting and cooling. 18.0 gms of a blend of PE and EPR copolymer analyzed for 7.1 mole % propylene and having a Mn of 2,000 and a Mw of 8,300 was recovered. A fractionation analysis was performed by stirring a 10 g portion of this solid product for one hour in 100 ml of toluene. The slurry was filtered and washed with 10 ml of fresh toluene. The copolymer in solution and the solid product were separately evaporated to dryness, weighed and analyzed by GPC and IR.

The soluble product (7.0g) had a Mn of 2,200 and a Mw of 11,900 and analyzed for 30 mole % propylene. The insoluble fraction had an Mn of 3000 and a Mw of 7,400 and analyzed to contain 4.8% propylene.

Example 3

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A 1-liter stainless steel pressure vessel, equipped with an incline blade stirrer, an external water jacket for temperature control, a septum inlet and vent line, and a regulated supply of dry ethylene, propylene and nitrogen, was dried and deoxygenated with a nitrogen flow. 400cc of dry, degassed toluene was introduced directly into the pressure vessel. 10cc of alumoxane molar (8.3 m moles in total aluminum) was injected into the vessel by a gas tight syringe through the septum inlet and the mixture was stirred at 1,200 rpms and 50°C for 5 minutes at zero (0) psig of nitrogen. 0.539 mg bis(methylcyclopentadienyl) zirconium dimethyl dissolved in 2.0 ml of dry, distilled toluene was injected through the septum inlet into the vessel. Similarly, 1.03 mg bis(pentamethylcyclopentadienyl) zirconium dichloride in 2.0 ml dry, distilled toluene was injected. The solution was saturated with 200cc propylene at a pressure of 111 psig for 15 seconds. Thereafter ethylene at 25 psig (C3/C, liquid ratio = 16) was passed into the vessel for 20 minutes while maintaining the temperature at 50°C at which time the reaction was stopped by rapidly venting and cooling. 30.0 gms of a blend of LLDPE and EP copolymer analyzed for 3.6% propylene and having a Mn of 5,600 and a Mw of 17,300 was recovered. The fractionation analysis, GPC & IR performed as in Example 2 yielded 3.0 gms of a soluble fraction having a Mn of 3,500, a \overline{M}_W of 16,000 and mole % of C_3^w of 20.6. The insoluble fraction (7.0 gms) had a Mn of 5,400, a Hw of 16,400 and mole % C_3 of 2.9%.

CLAIMS:

- 1. A catalyst system for the production of reactor blend polymers, said catalyst comprising (a) at least two different organometallic coordination compounds which are derivatives of mono, di or tricyclopentadienyls with Group 4b, 5b and 6b transition metal, the compounds having different reactivity with respect to the monomers employed and (b) an alumoxane.
- 2. A homogeneous catalyst system for the production of reactor blend polymers comprising a blend of polyethylene and an ethylene-olefin copolymer; said catalyst comprising:
 - (a) at least two metallocenes having represented by the-general formula $(C_5R')_pR''_s(C_5R'_m)MeQ_{3-p} \text{ or } \\ R''_s(C_5R'_m)_2MeQ' \text{ each having different } \\ \text{reactivity ratios, and }$
 - (b) an alumoxane wherein (C5R'm) is a cyclopentadienyl or substituted cyclopentadienyl, each R' which can be the same or different is hydrogen or a ·R· hydrocarbyl radical or two substituents together form a fused C4-C6 ring, R" is a C_1 - C_4 alkylene radical, a dialkyl germanium or silicone, or an alkyl phosphine or amine radical bridging two (C5R'm) rings, Q is a hydrocarbon radical or halogen and can be the same or different, Q' is an alkylidene radical having from 1 to 20 carbon atoms, Me is a transition metal of Group 4b, 5b and 6b, s is 0 or 1, p is 0, 1 or 2; when p = 0, s = 0; m is 4 when s is 1; m is 5 when s is 0.
 - 3. The catalyst system of claim 2 wherein Q is methyl, phenyl or chloride.

- 4. The catalyst system of claim 2 or claim 3, wherein Me is selected from zirconium and titanium.
- 5. The catalyst system of claim 4 comprising at least 2 zirconocenes.
- 6. The catalyst system of claim 4 comprising at least 1 titanocene and 1 zirconocene.
- 7. The catalyst system of claim 5 comprising bis (methylcyclopentadienyl) zirconium dichloride and bis (pentamethylcyclopentadienyl) zirconium dichloride.
- 8. A process for producing a reactor blend comprising polymerizing ethylene and at least alpha-olefin simultaneously in the presence of the catalyst system of any of claims 1 to 7.
- 9. The process of claim 8 wherein the polymer blend comprises a blend of polyethylene and copolyethylene-propylene.
- 10. The process of claim 9 wherein the polyethylene is LLDPE or HDPE.



EUROPEAN SEARCH REPORT

EP 84 30 3806

1	DOCUMENTS CONSIDERED TO BE I Citation of document with Indication, where appro		CLASSIFICATION OF THE
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